

**Effects of transfer processes on marine atmospheric
boundary layer**

or

**Effects of boundary layer processes on air-sea
exchange**

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Effect of transfer process on MABL

Swell

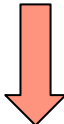
Long waves
create
form drag



Upward momentum flux



Quasi-frictional decoupling
at the surface



MABL

Turbulence resembles free
convection conditions

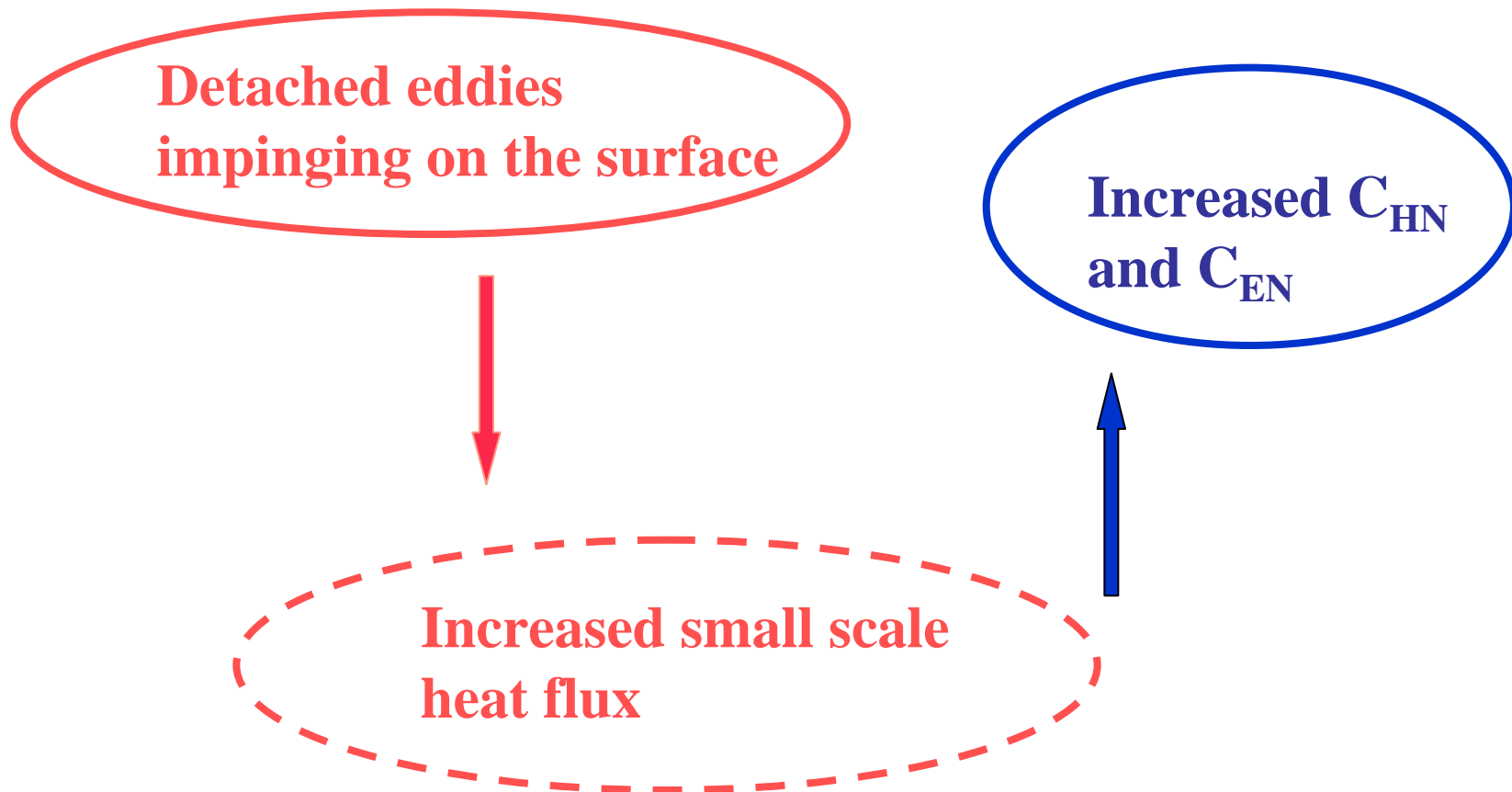
Ocean

Effect of MABL process on air-sea exchange

UVCN regime

MABL

Ocean



**In models air-sea exchange
is described through Monin-Obukhov similarity
theory
a theory which is well tested over land**

but

is it valid over the ocean?

What are the differences ?

Large heat capacity

Small diurnal variation

**Roughness (waves)
increasing with
increasing wind speed**

Long term measurements in the Baltic Sea

2 buoys (temp, wave height, dir. and CO₂)

Footprint area

100°

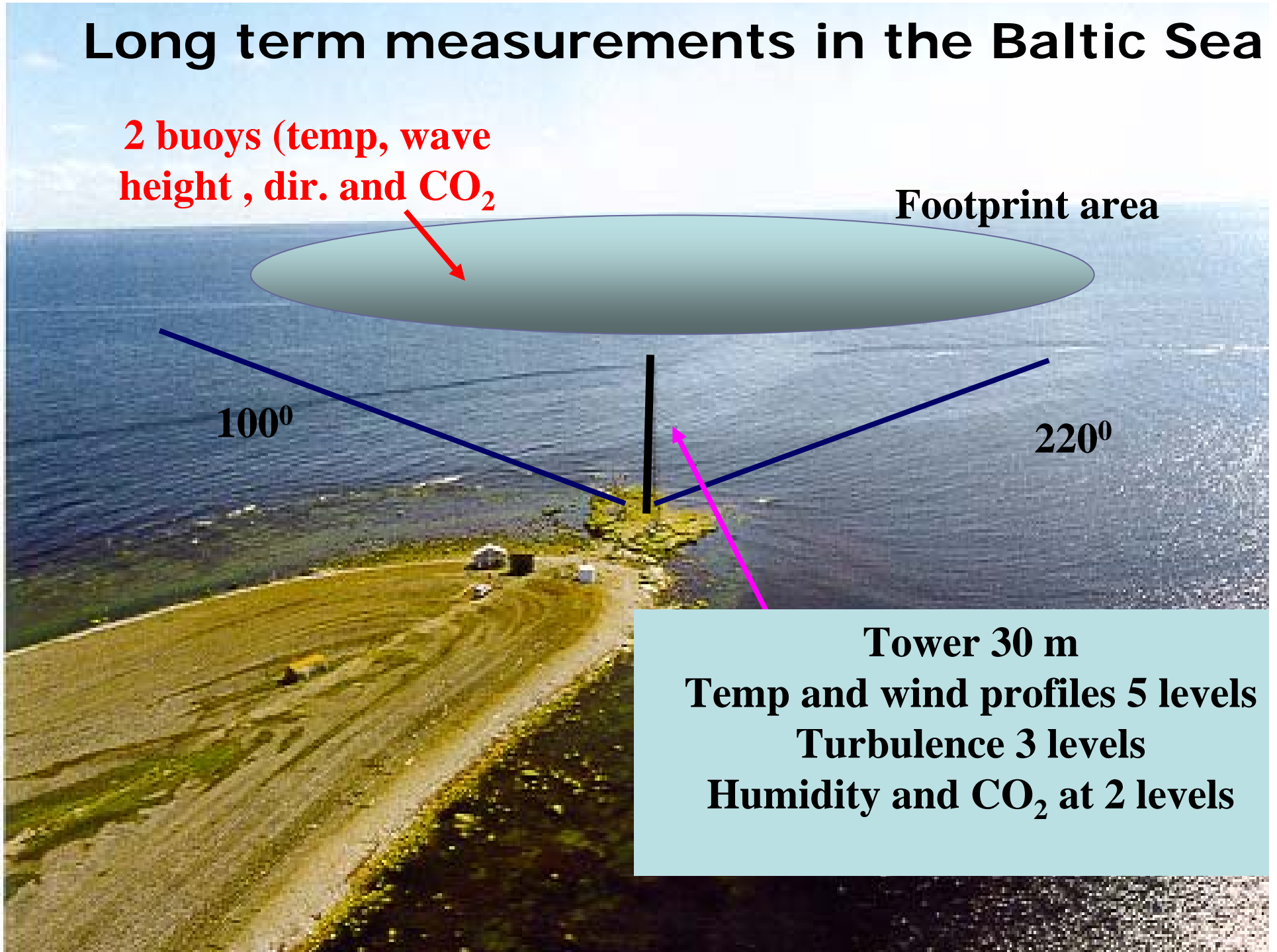
220°

Tower 30 m

Temp and wind profiles 5 levels

Turbulence 3 levels

Humidity and CO₂ at 2 levels



Short term experiments with RV Aranda and ASIS buoy

Turbulence, wind speed, temperature and wave parameters



In the mean, excellent agreement between tower and ASIS

Data set from Agile experiment in lake Ontario 1994-95

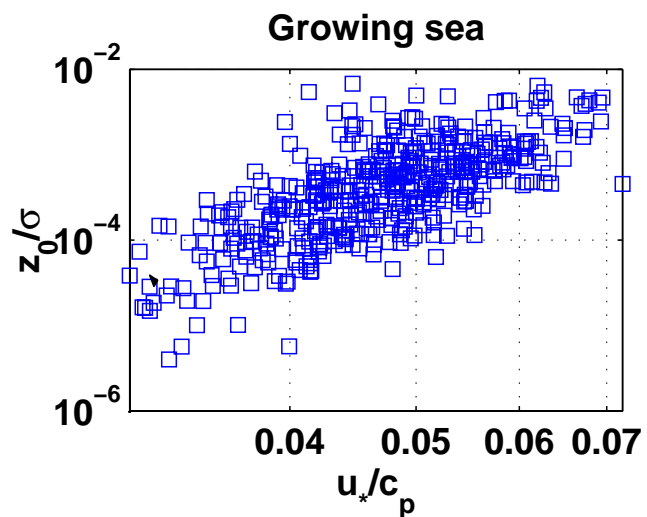
**A 15- m research vessel Agile was equipped to measure waves
and turbulence with**

- Sonic R2A**
- Thermocouple**
- Licor**
- Wave staff array**

**Measurements were performed at 7.8 m during two
autumn periods**

Growing sea (slow waves) Unstable stratification

- Monin-Obukhov similarity theory is valid
but
roughness length, z_0 , is a function of wave age



Swell
(long waves traveling faster than the wind)
and
unstable stratification

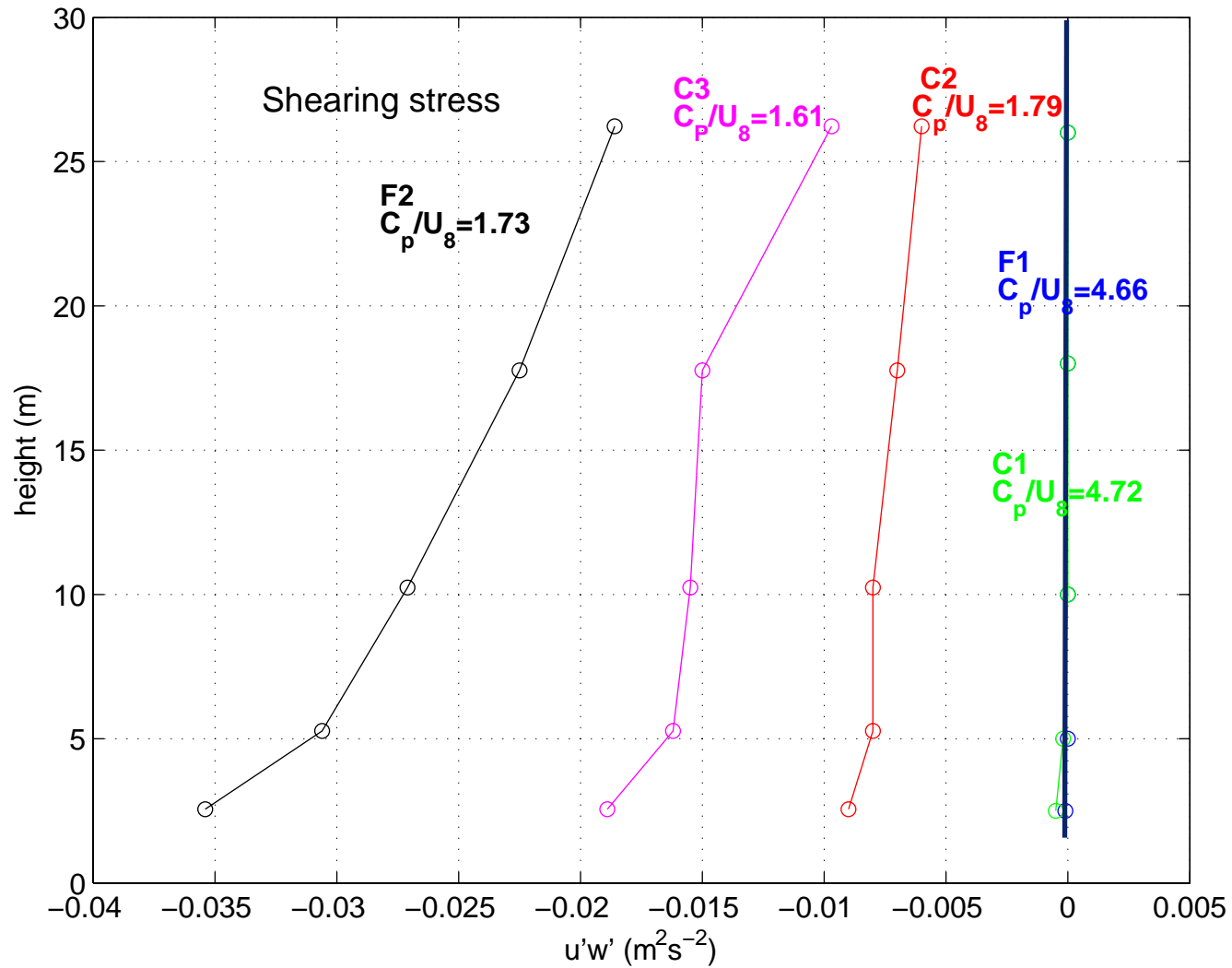
- **A quite different type of boundary layer develops**

The swell driven BL is characterized by

- Small or positive momentum flux
- Low level jet
- M-O scaling does not hold
- The vertical extent can be global
- Turbulence spectra resemble free convection conditions
- Swell represents **reverse** atmospheric-ocean coupling



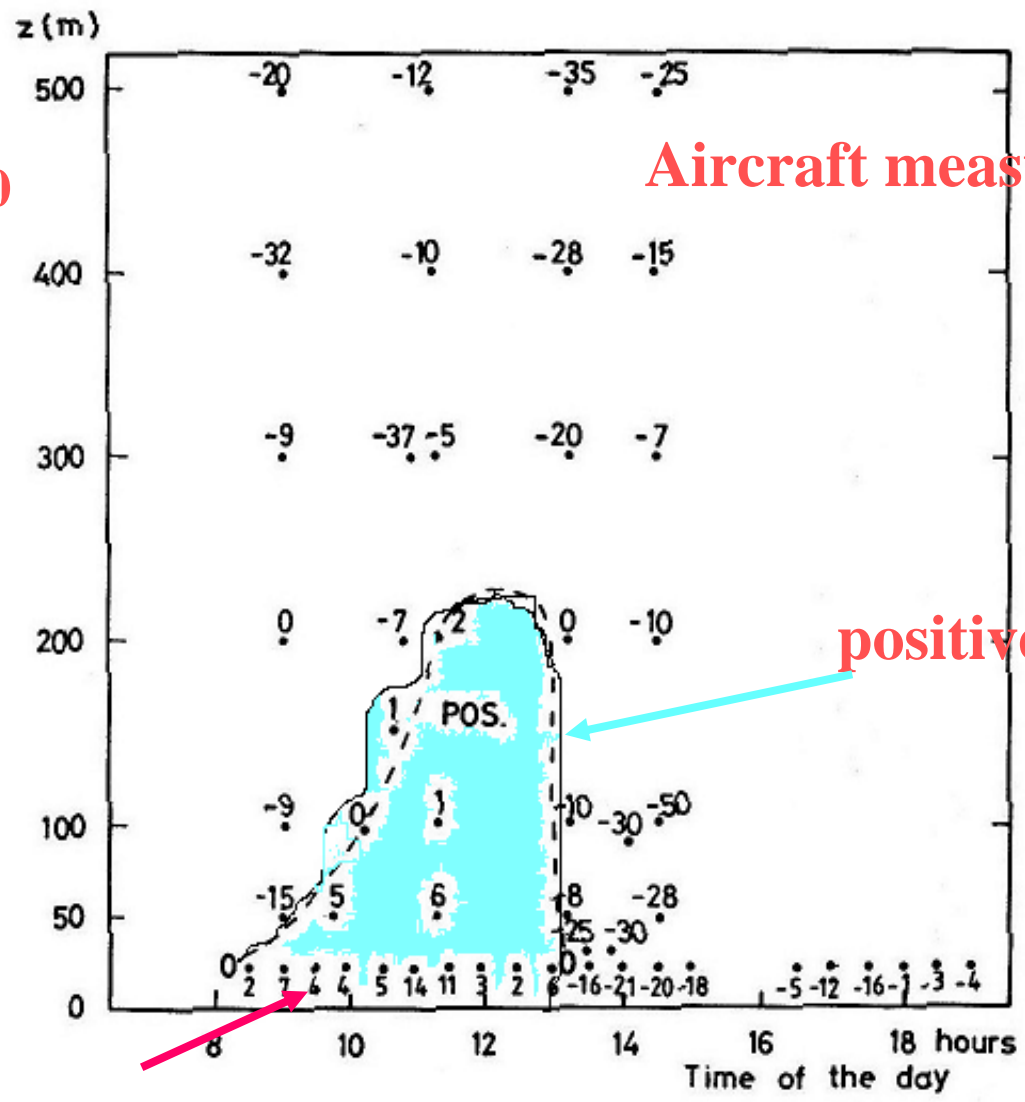
Small momentum flux



Positive momentum flux

uw x 1000

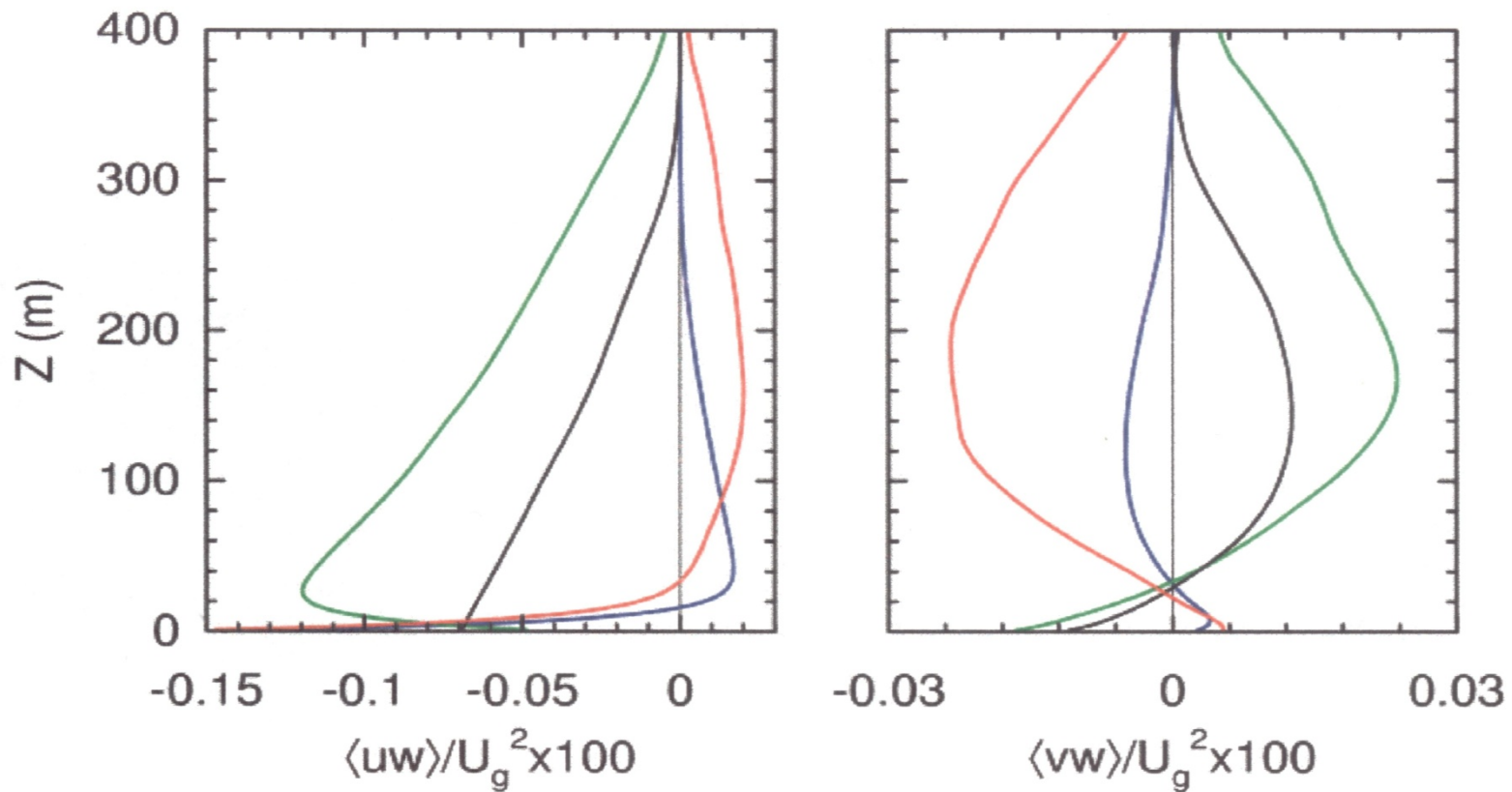
Aircraft measurements



Tower measurements

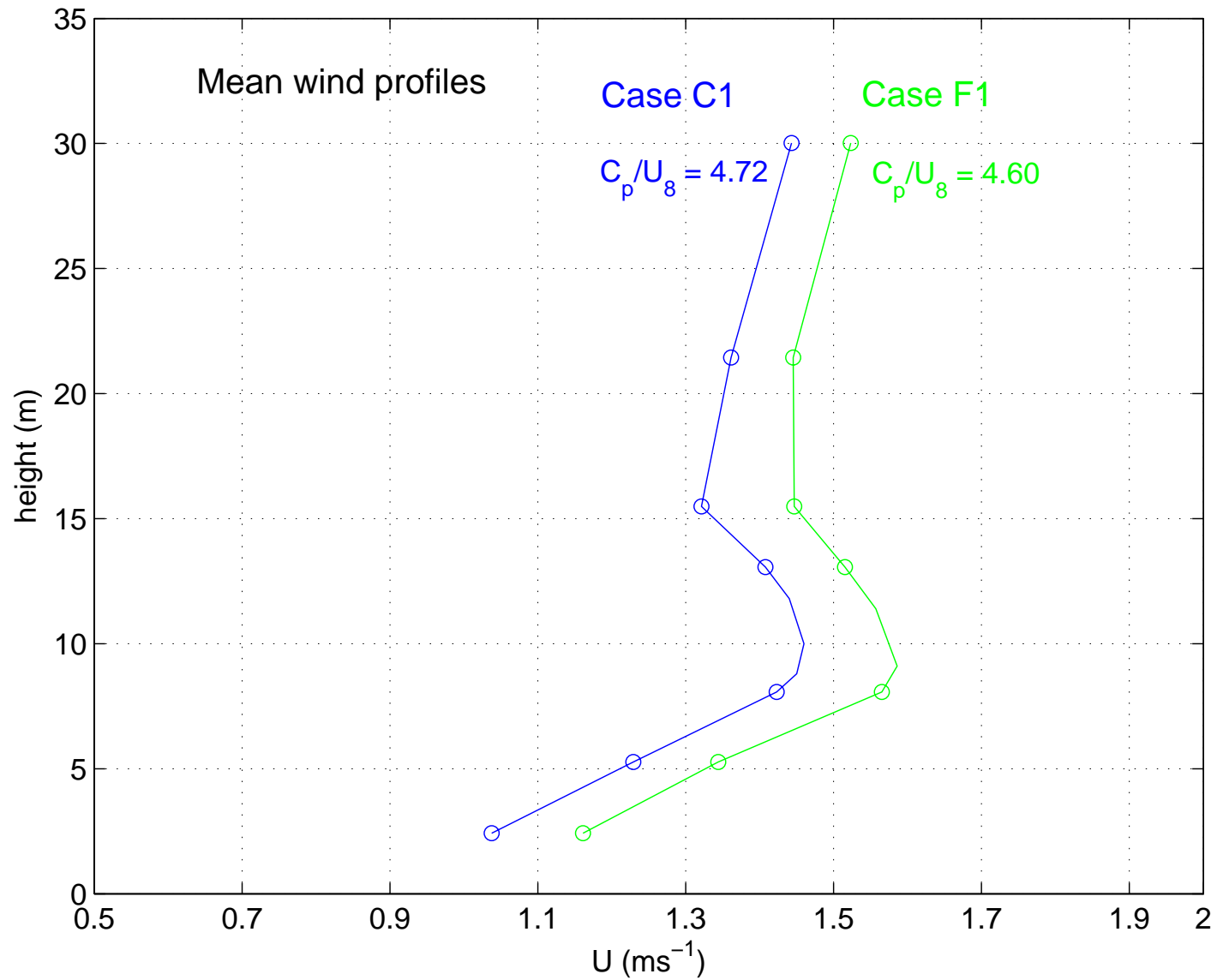
positive uw

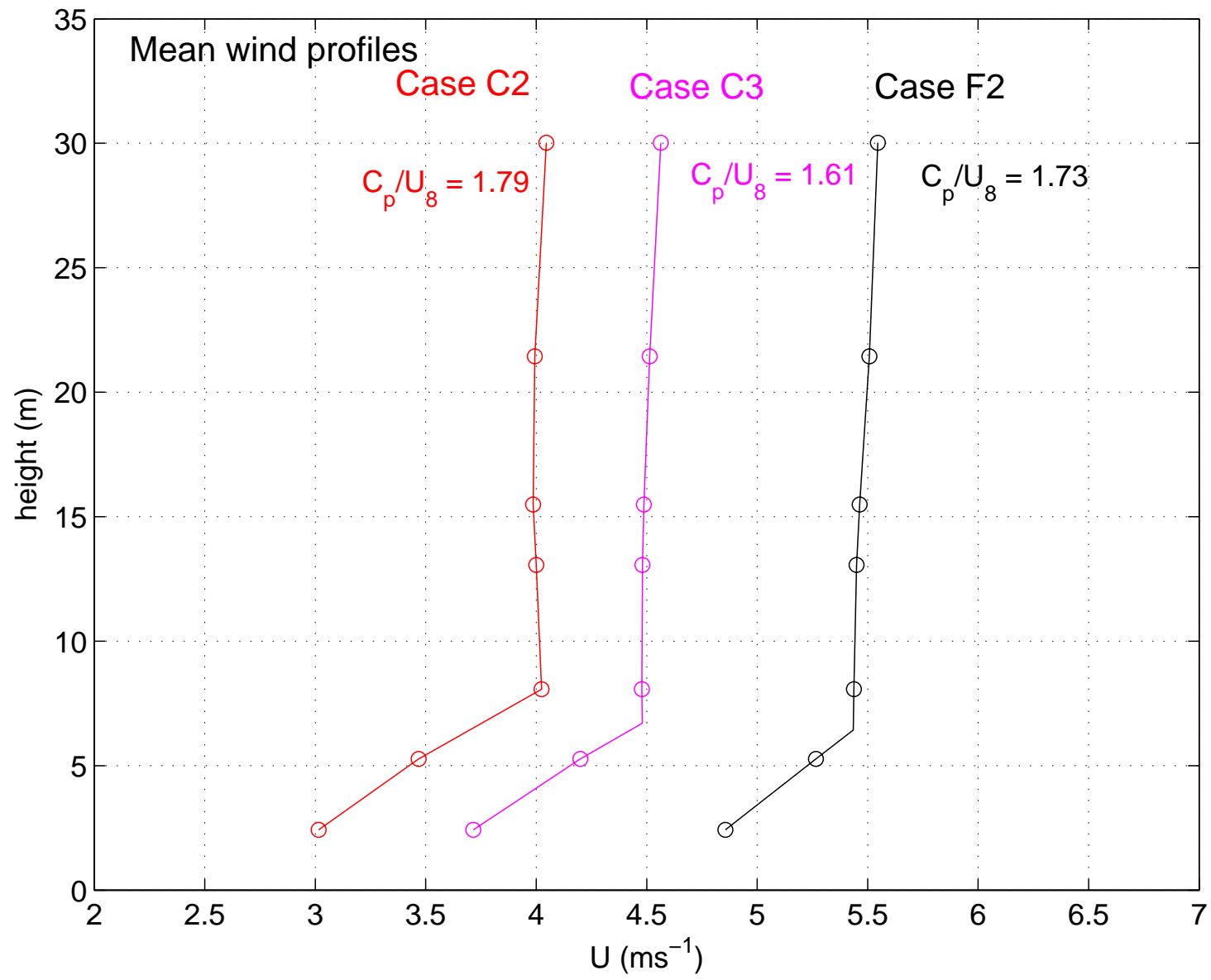
LES simulations Peter Sullivan



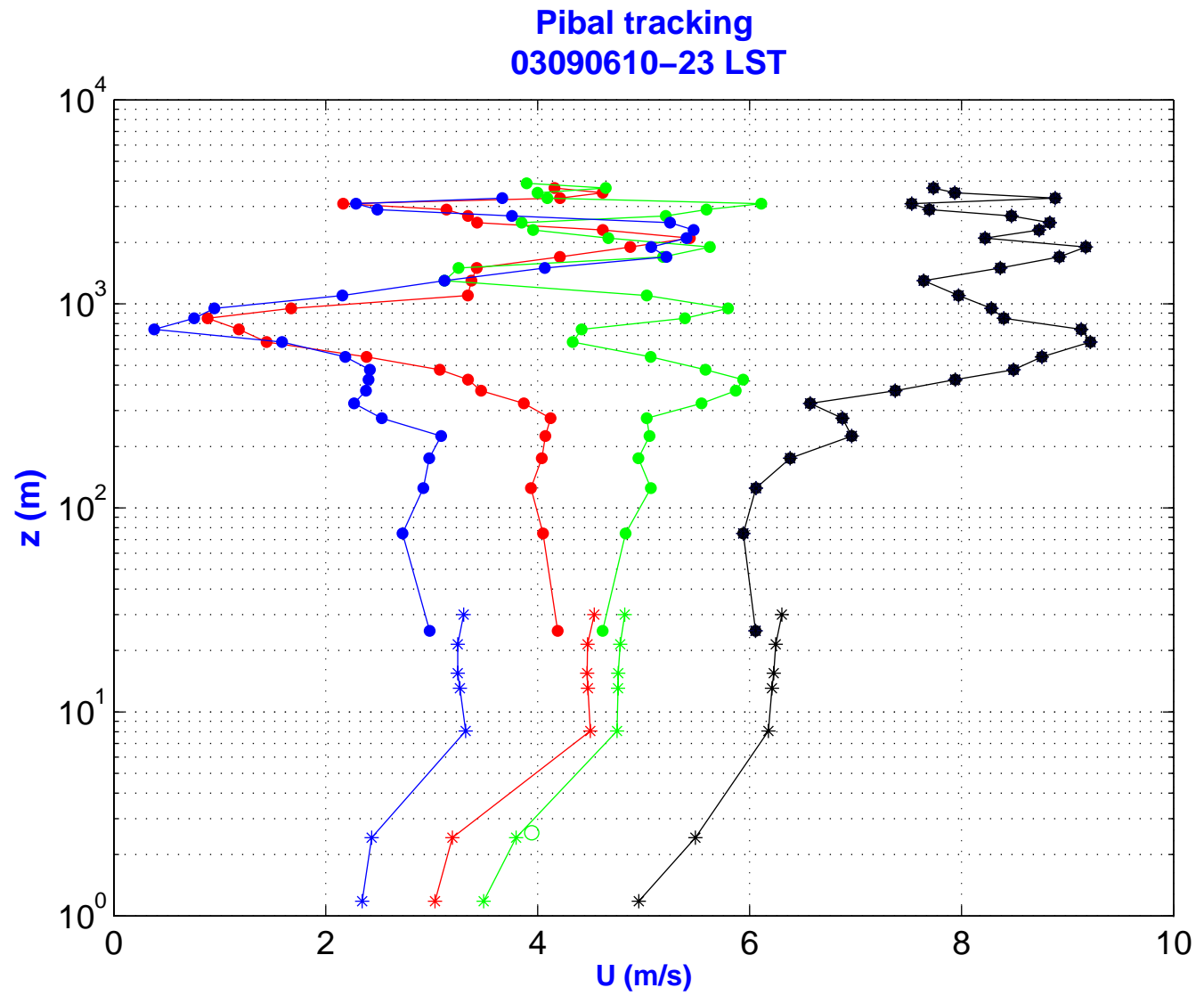
- Small z_o
- Stationary wave
- Fast wave, weak wind
- Fast wave, weak wind, unstable

Low level jet

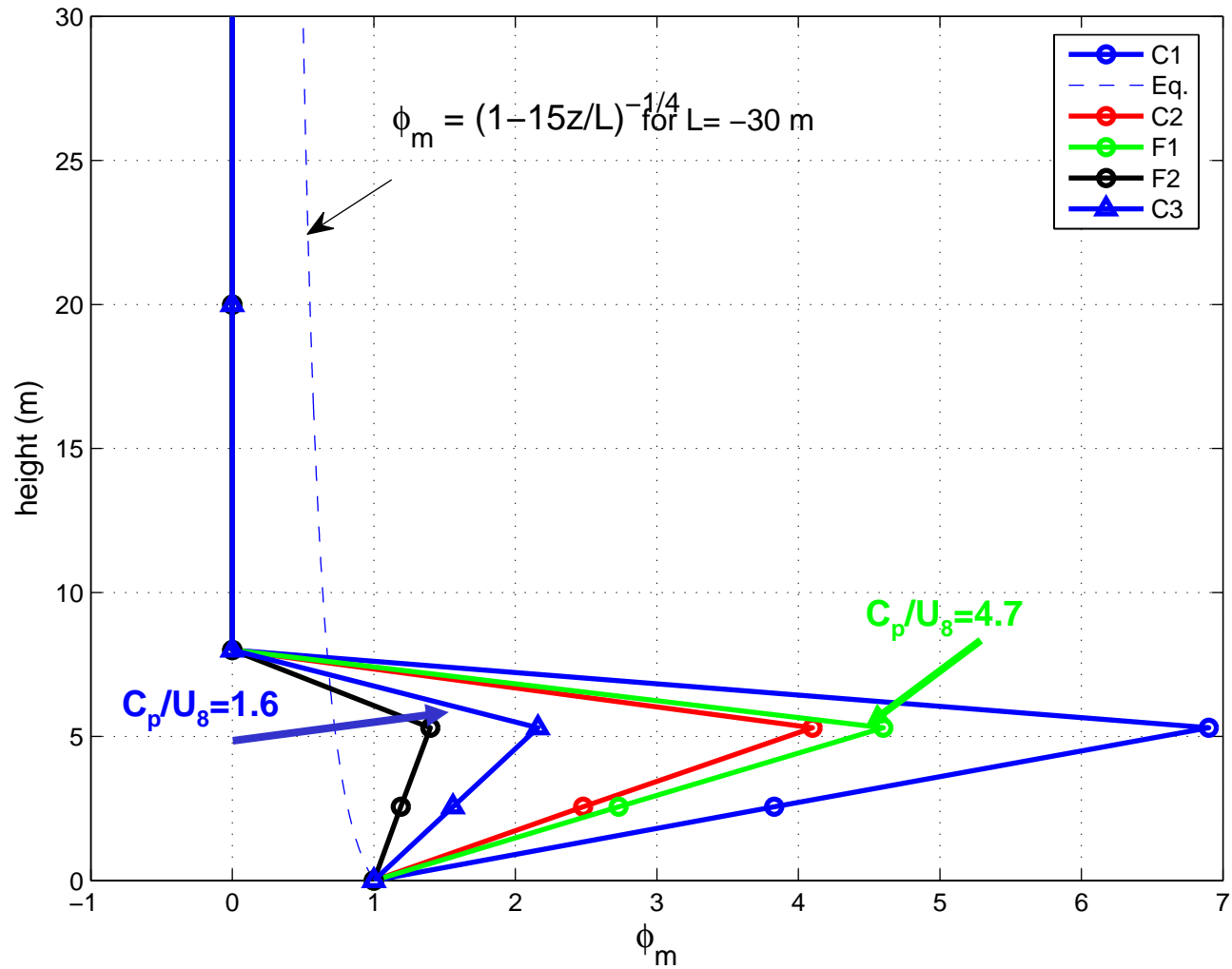




The vertical extent is global



Φ_m calculated for five swell cases



Turbulent kinetic energy budget

$$0 = \overline{u'w'} \cdot \frac{\partial U}{\partial z} - \frac{g}{T_o} \overline{w'\theta} + \frac{1}{\rho_o} \cdot \frac{\partial \overline{pw'}}{\partial z} + \frac{\partial \overline{w'e}}{\partial z} + \varepsilon$$

P

B

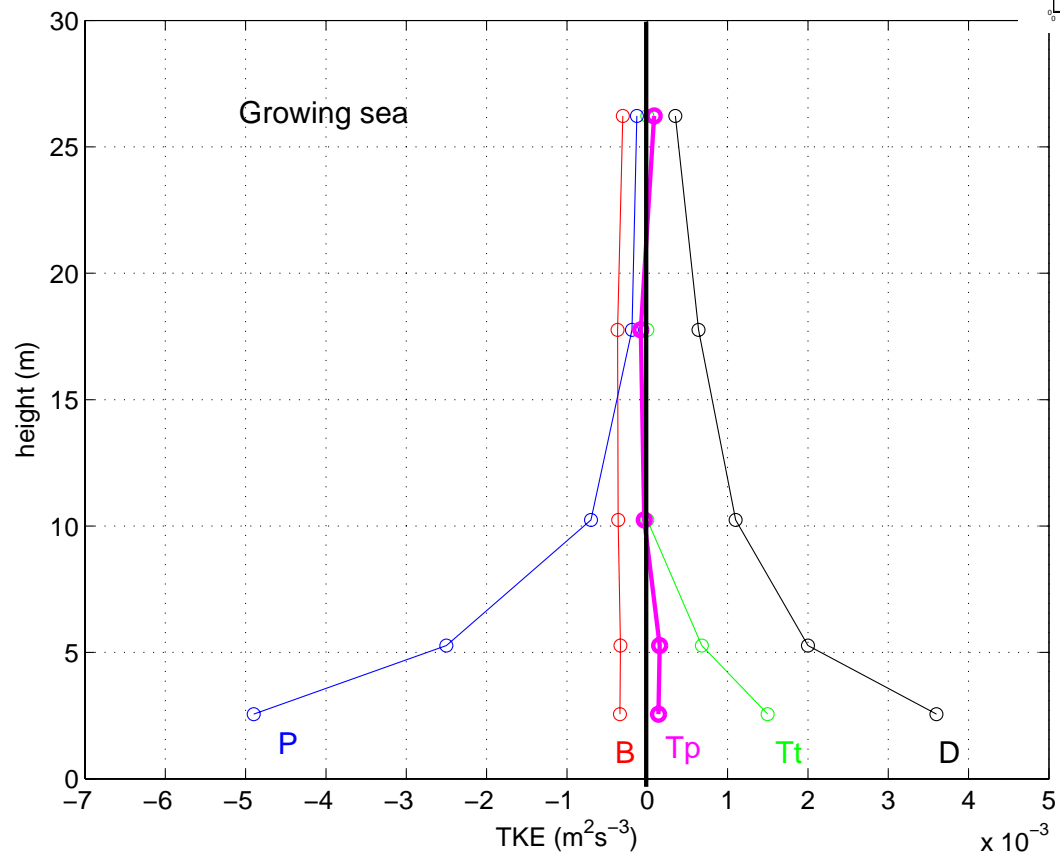
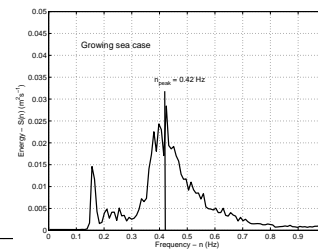
T_p

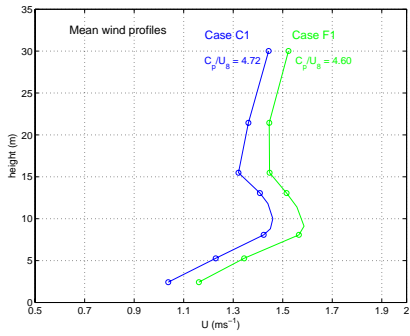
T_t

D

Turbulent energy budget

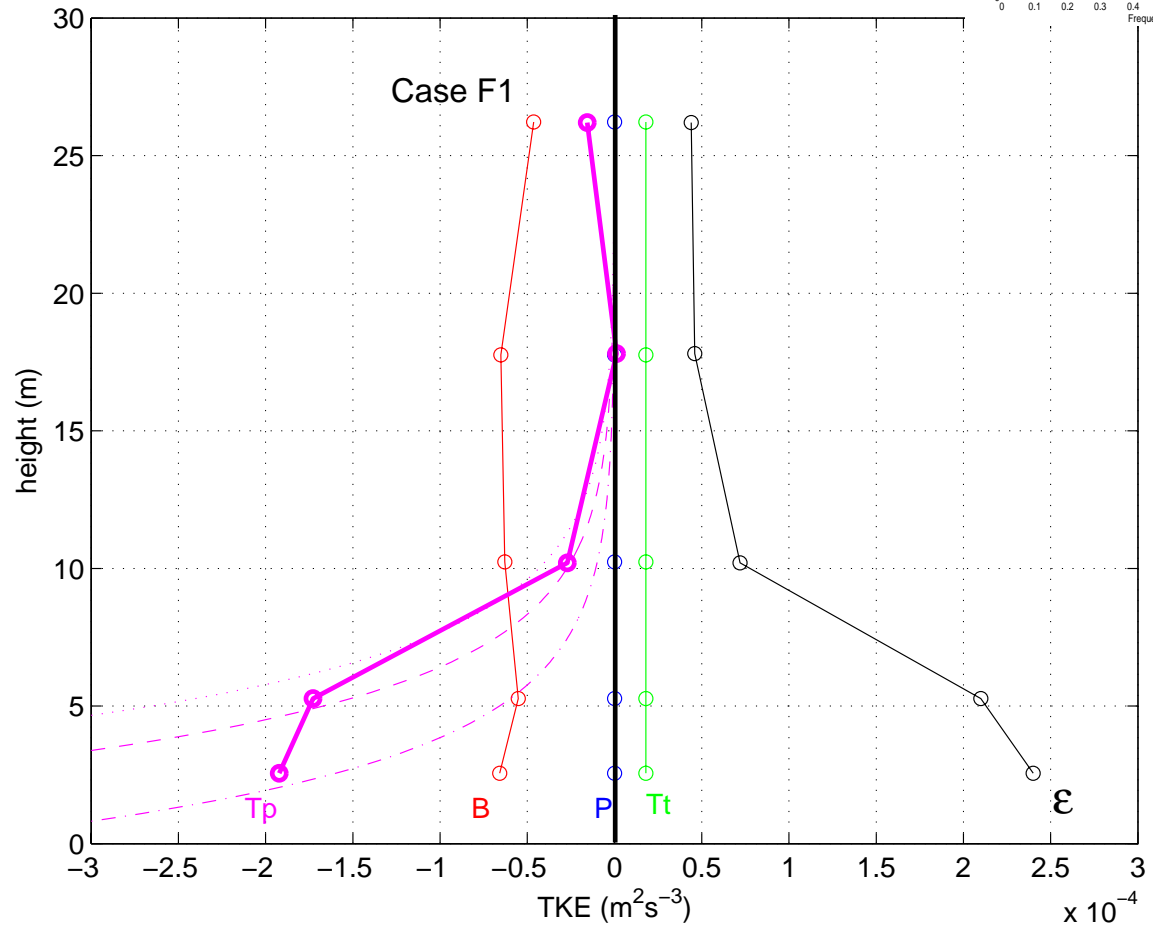
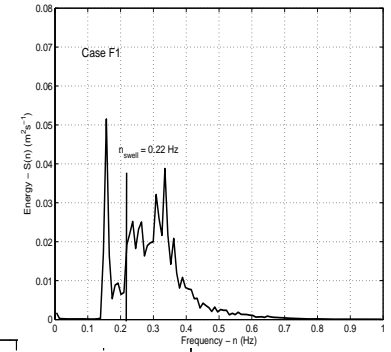
Growing sea

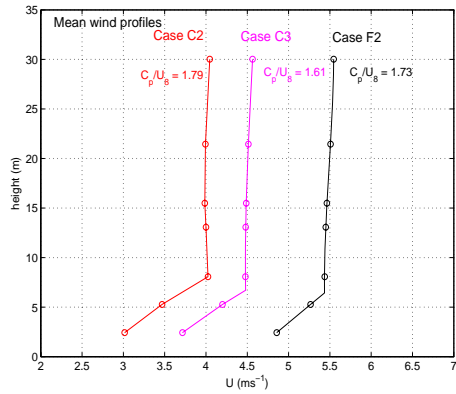




Turbulent energy budget

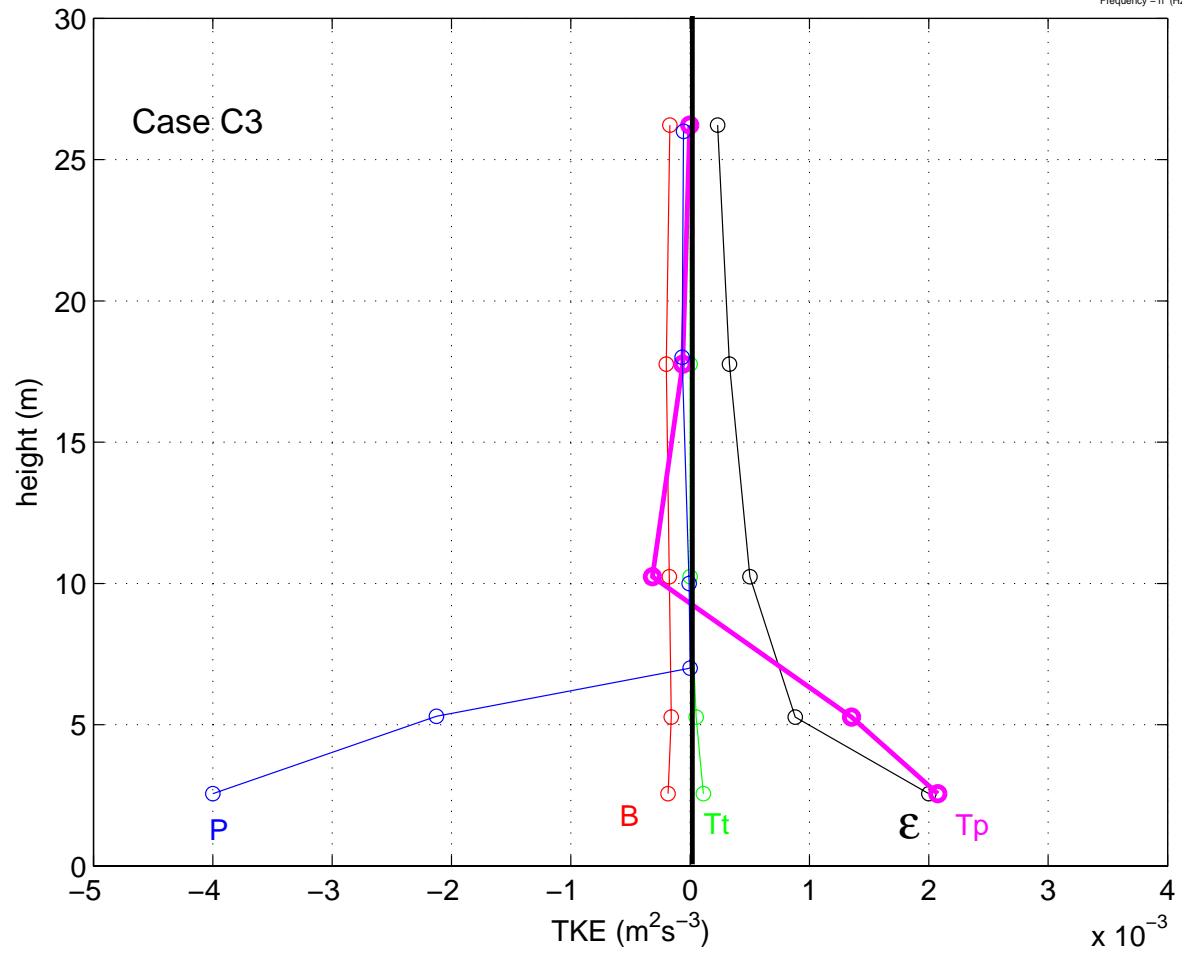
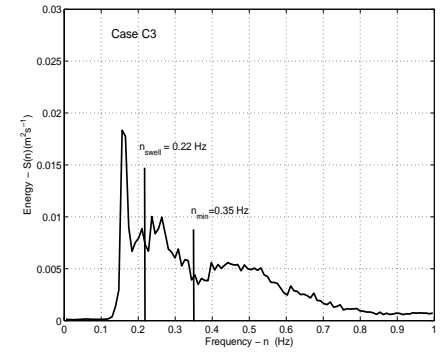
$c_p/U=4.7$





Turbulent energy budget

$c_p/U=1.6$



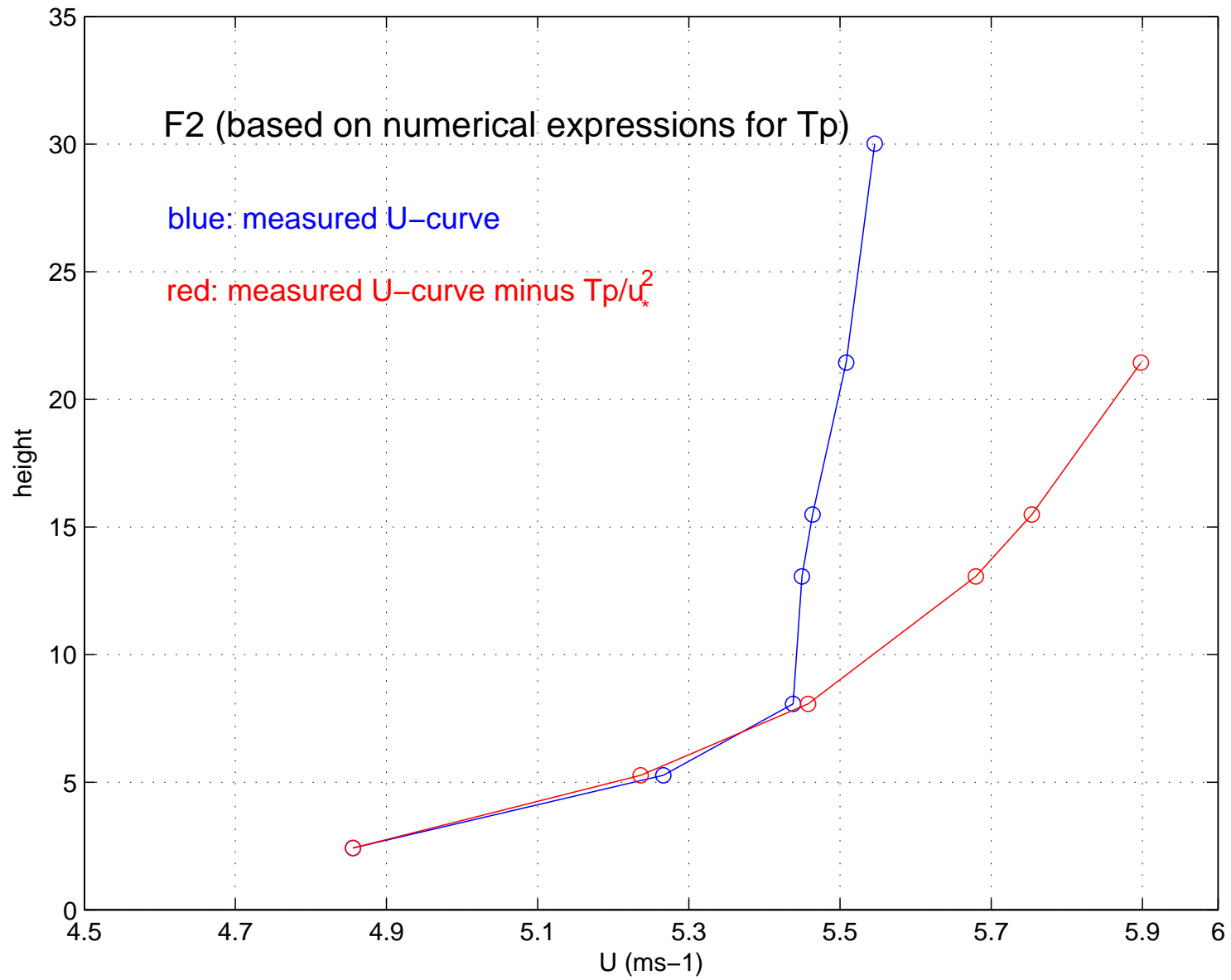
From the turbulence energy eq,

$$\frac{\partial U}{\partial z} = -\frac{1}{u'w'} \left(-\frac{g}{T} \overline{w'\theta_v'} + \frac{\partial}{\partial z} \frac{\overline{w'q'^2}}{2} + T_p + \varepsilon \right)$$

The effect of T_p can be isolated

$$\left(\frac{\partial U}{\partial z} \right)_{T_p} = -\frac{T_p}{u'w'}$$

$$U(z) - U(2.5m) = \int_{2.5m}^z \frac{T_p}{u_*^2} dz$$



Heat fluxes

All turbulent fluxes in models must be expressed as mean variables

Stanton number

$$C_H = \frac{\overline{w'\theta'}}{U(T_o - T_s)}$$

Heat flux

Wind speed

Air-sea temperature difference

The diagram illustrates the Stanton number equation, $C_H = \frac{\overline{w'\theta'}}{U(T_o - T_s)}$. A red arrow points from the text 'Stanton number' to the symbol C_H . Three blue arrows point from descriptive text to parts of the equation: 'Heat flux' points to the numerator $\overline{w'\theta'}$, 'Wind speed' points to the denominator U , and 'Air-sea temperature difference' points to the denominator $(T_o - T_s)$.

In the same way for latent heat, C_E

Reduced to neutral stability

$$C_{HN} = \frac{\kappa^2}{\{\ln(z/z_0)\}\{\ln(z/z_{0T})\}}$$

Von Karman constant=0.4

Roughness length

Roughness length for temperature

The diagram shows the equation $C_{HN} = \frac{\kappa^2}{\{\ln(z/z_0)\}\{\ln(z/z_{0T})\}}$. Three blue arrows point from text labels to parts of the equation: one from 'Von Karman constant=0.4' to κ^2 , one from 'Roughness length' to $\ln(z/z_0)$, and one from 'Roughness length for temperature' to $\ln(z/z_{0T})$.

In the same way for latent heat, C_{EN}

Heat fluxes, unstable stratification

$$\Delta T > 3^\circ$$

- **Traditional parametrization (COARE algorithm) is valid**
- **No variation with wave age**

Heat fluxes, stable stratification

- **Low-level jets cause shear suppression leading to decreased fluxes**

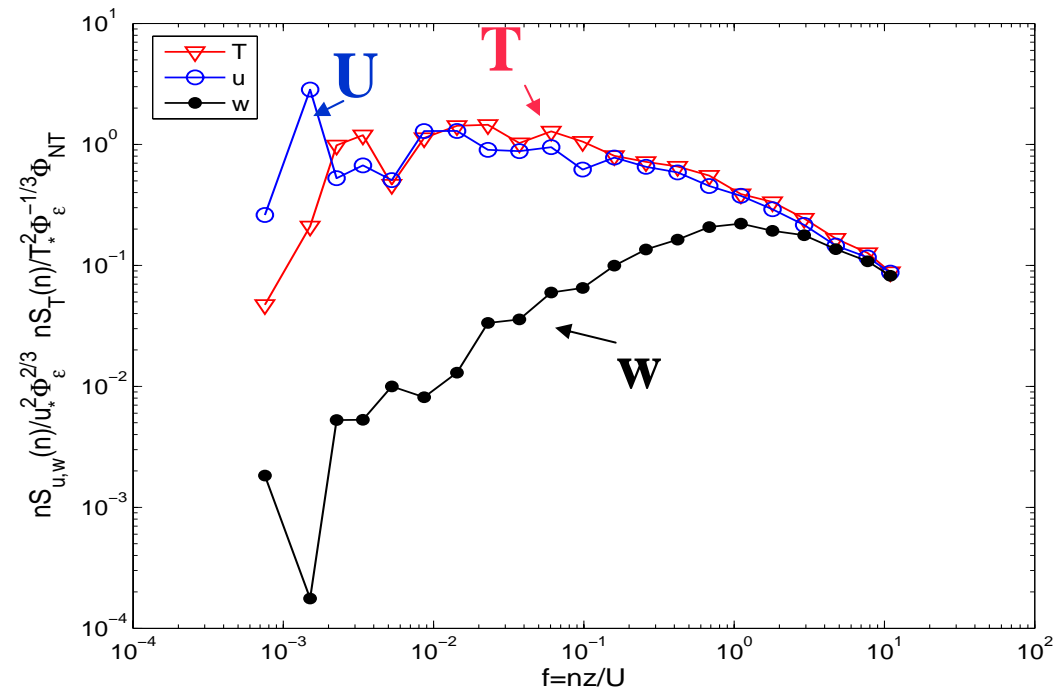
**Heat fluxes, unstable stratification, very close to
neutral**

Wind speed > 10 m/s and $\Delta T < 3^\circ$

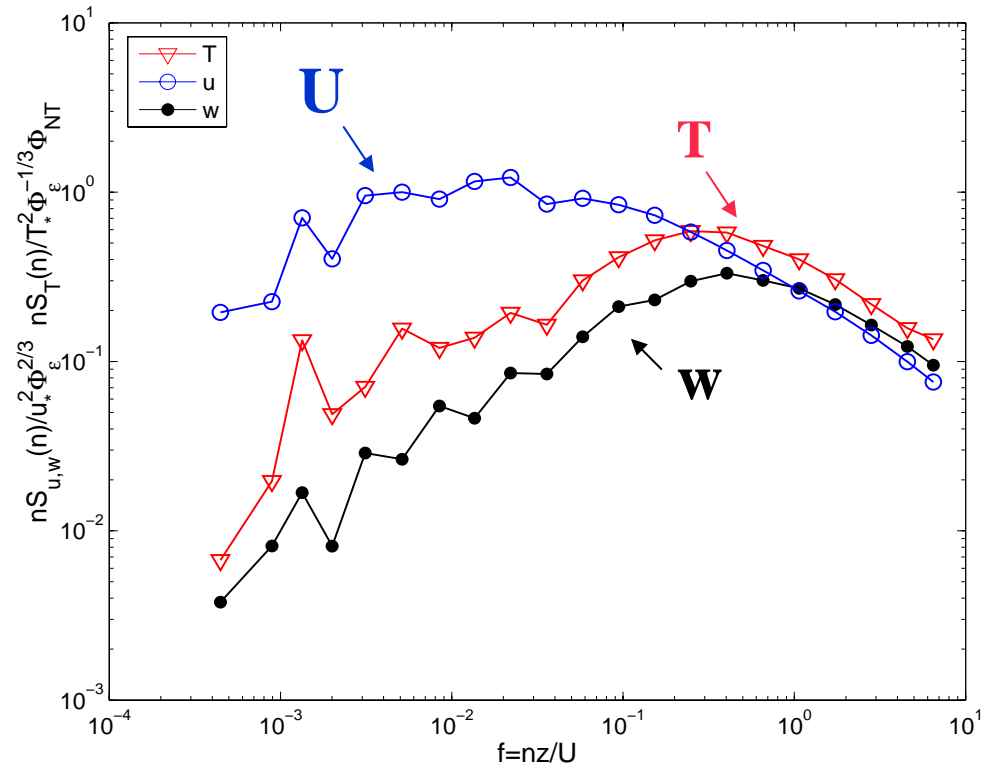


Fluxes are underestimated with COARE algorithm

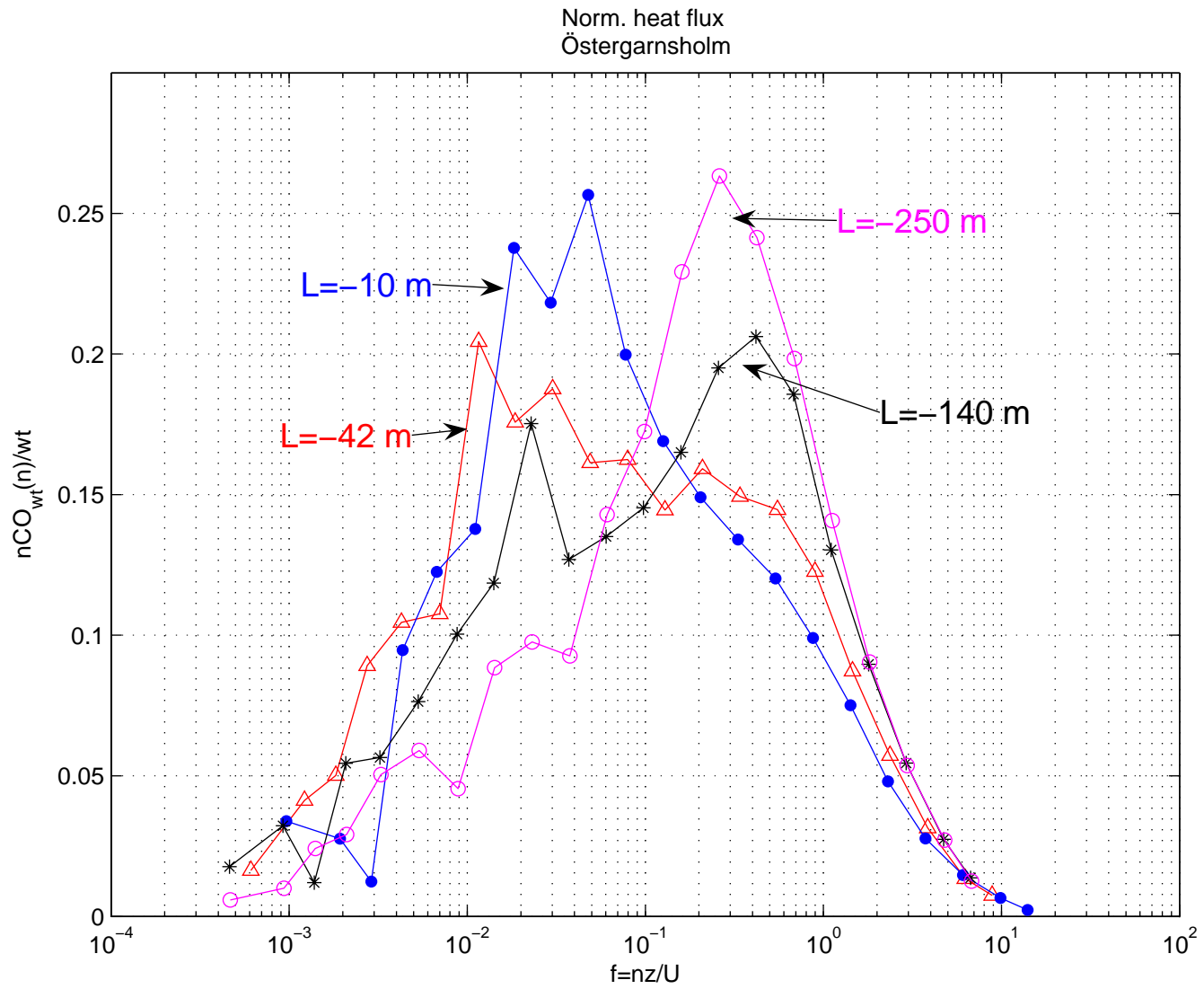
Unstable stratification -- horizontal rolls



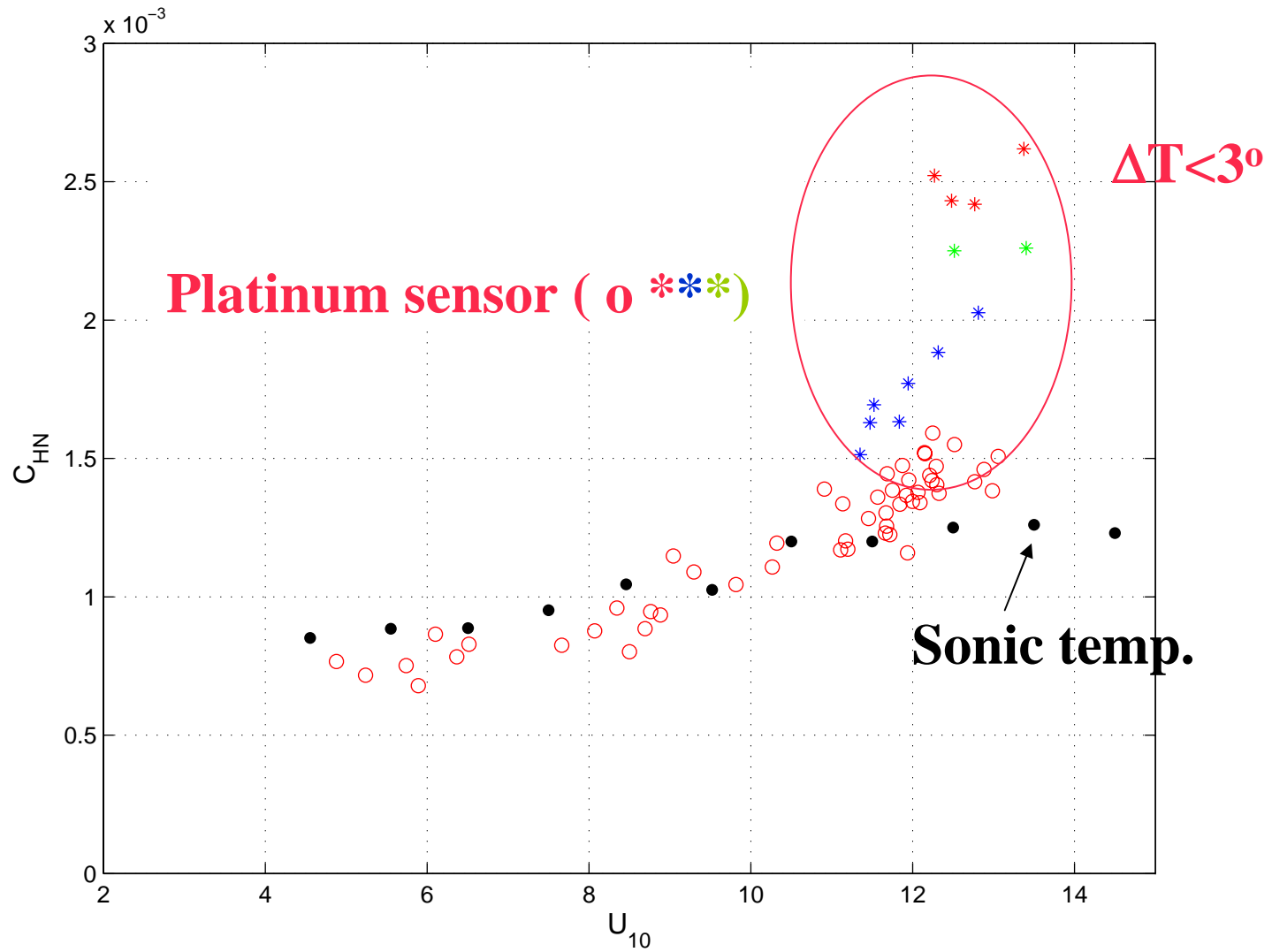
Unstable near neutral -- detached eddies



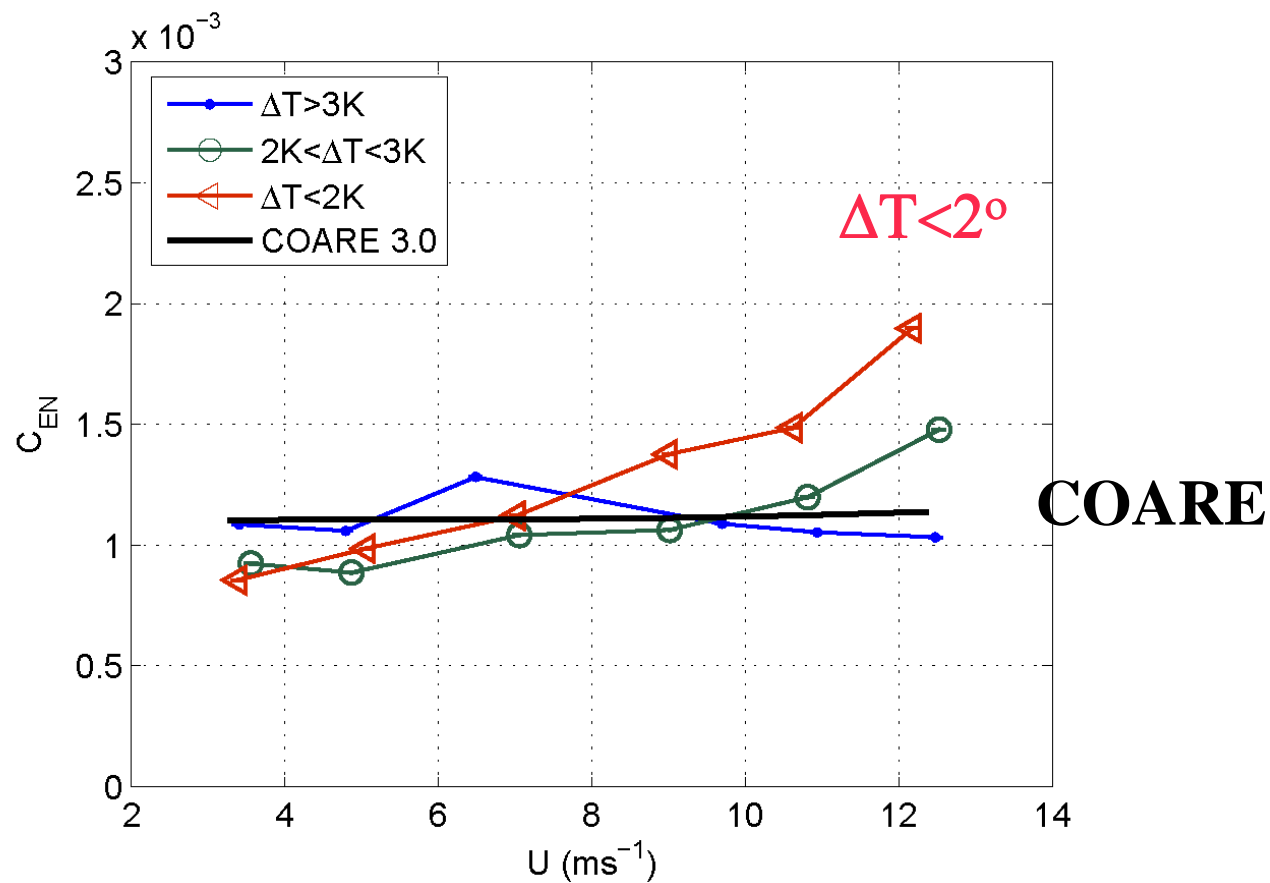
Normalized heat fluxes



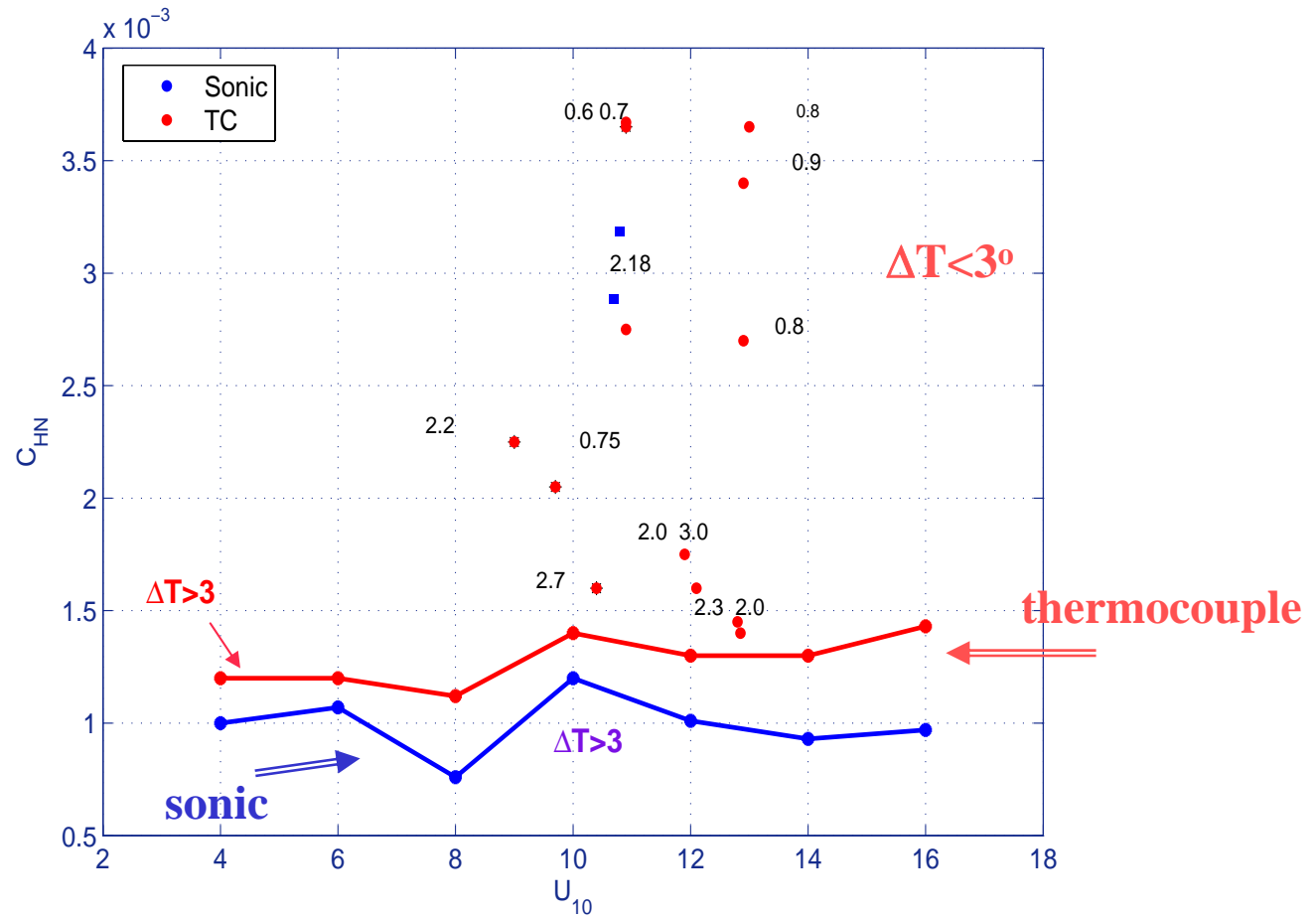
Heat flux from Östergarnsholm



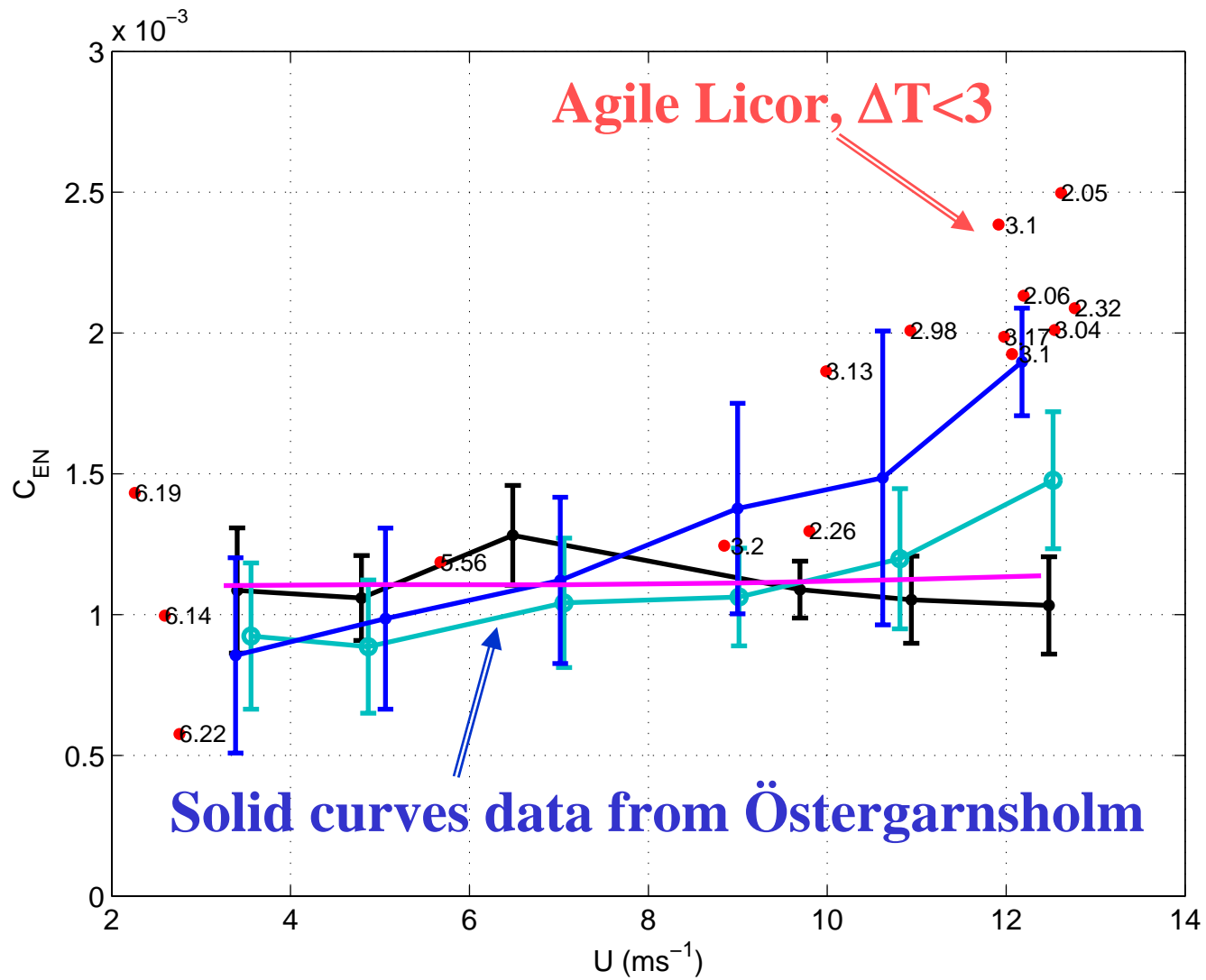
Latent heat flux, Östergarnsholm



Agile heat flux

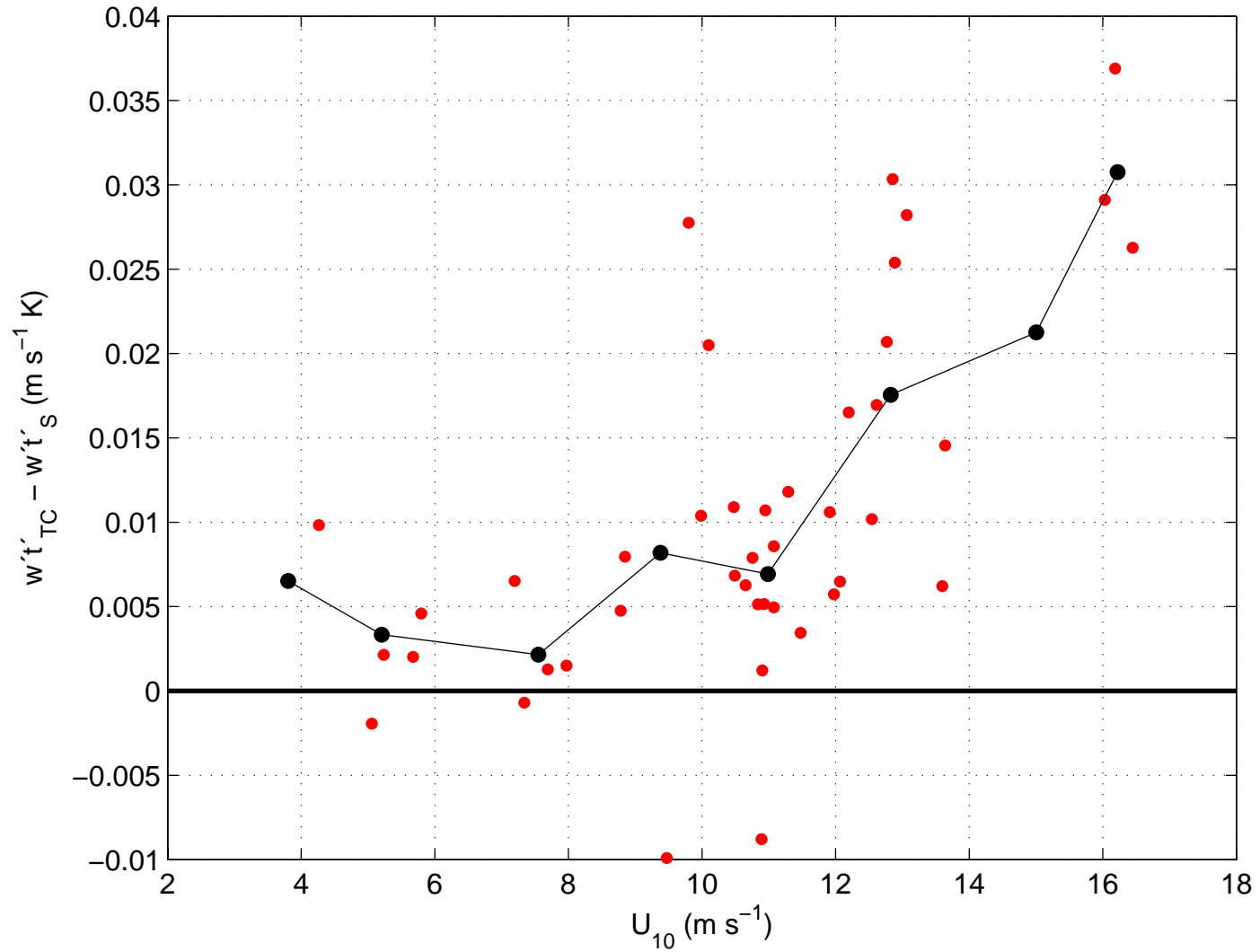


Agile latent heat flux



Agile heat flux: $(wt)_{TC} - (wt)_{sonic}$

Comparison of heat fluxes, differences, Agile-94,95

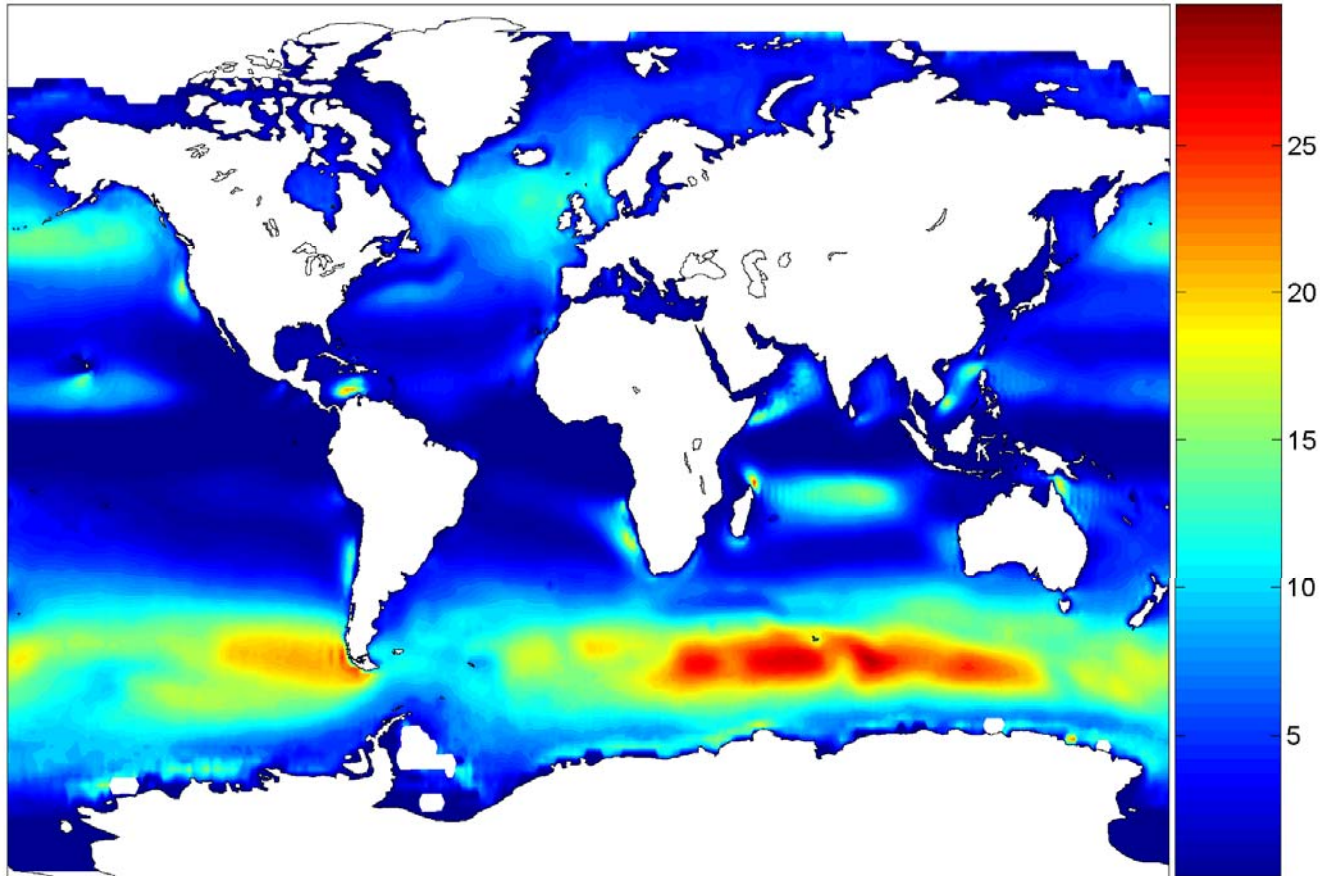


The **unstable very close to neutral regime**

- **The UVCN regime is defined for $\Delta T < 3^\circ$ and $U > 10 \text{ m/s}$**
- **It is found both over land and sea in the lowest region ($z < 15 \text{ m}$) of the surface layer**
- **Small scale heat flux is a result of detached eddies originating from the upper part of the surface. This is in contrast to a convective surface layer ruled by horizontal rolls.**

Frequency (%) of occurrence of UVCN conditions

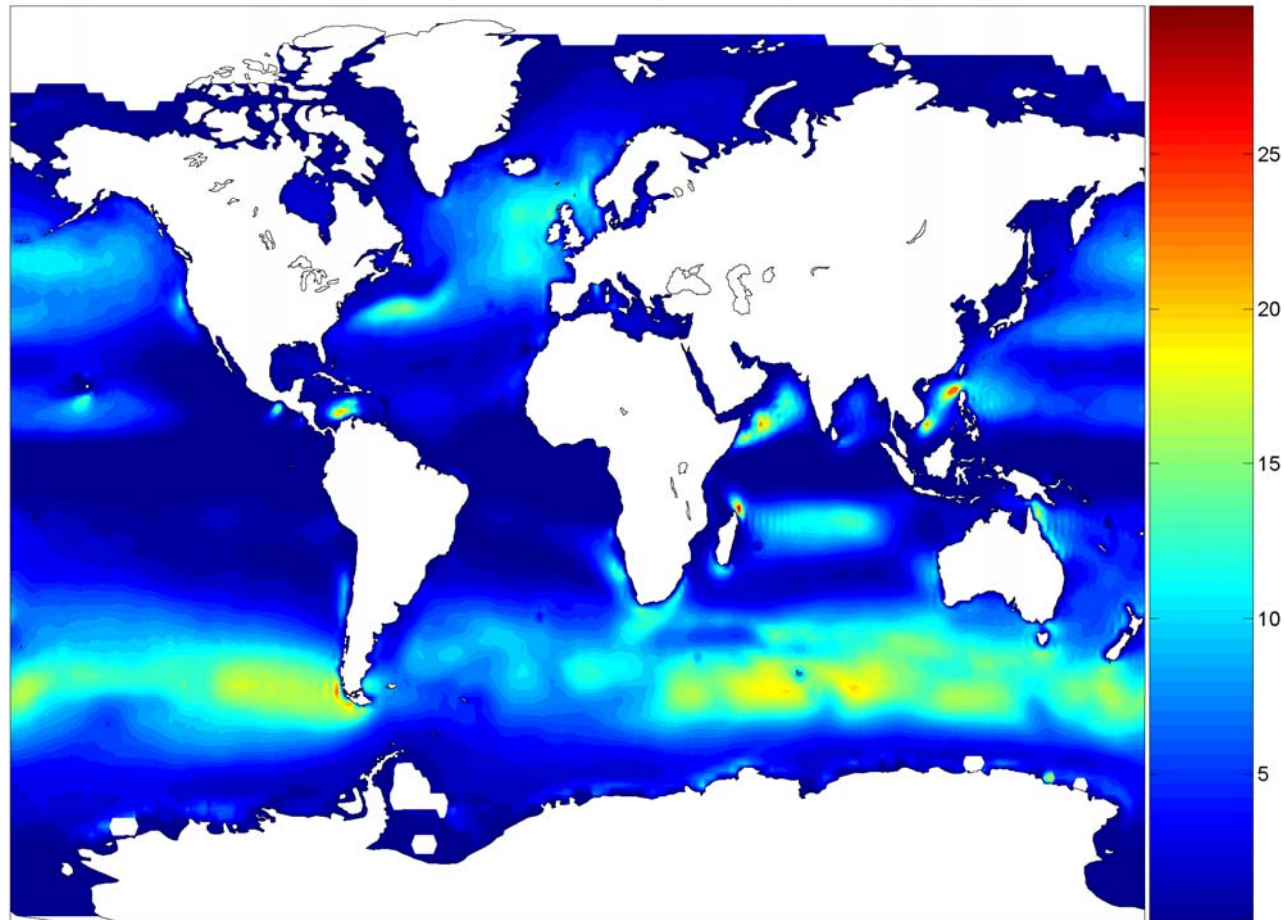
Relative frequency of occurrence of UVCN conditions, 1979–2001, (%)



ERA-40 reanalysis

Increase (W/m^2) in latent heat flux with UVCN regime included

Mean difference in latent heat flux, uvcn-no uvcn, RCS07 param. (W/m^2), 1979–2001



ERA-40 reanalysis

Global mean values of the increase of heat fluxes with UVCN regime included

- Sensible heat flux = 0.8 W/m^2
- Latent heat flux (evaporation) = 2.4 W/m^2
- The effect of increased anthropogenic greenhouse gases (2006) on net radiation = $2.63 \pm 0.26 \text{ W/m}^2$

Conclusions

Unstable stratification

- **M-O similarity theory is only valid for growing waves**

During swell the MABL is characterized by

- **Low-level jet (LLJ) at 5-10 m height**
- **Constant wind speed above LLJ**
- **Small or positive momentum flux varying with height**
- **Energy is transported from waves to atmosphere by pressure transport term T_p**

Mixed seas

As soon as a small portion of the waves are travelling faster than the wind (mixed seas) MABL is slowly changing from an ordinary boundary layer to a 'swell dominated ' boundary layer and

Monin-Obukhov similarity theory is not valid

During **stable stratification** wave effects are small

Heat fluxes

- The dynamics of the MABL influence the air-sea exchange of sensible and latent heat.
- When the convective boundary layer is ruled by horizontal rolls the well known COARE algorithm is valid.
- When detached eddies originating from the upper part of the surface layer is present (UVCN regime) the heat fluxes are increased and the Φ_h -function goes to zero

Why has not the UVCN regime been observed earlier?

- **sonic temperature fails to measure temperature fluctuations correctly when σ_T is small (high wind speed, small ΔT)**
- **data with small ΔT are often removed from the data set**
- **measurements are taken at heights above the UVCN layer.**

Thanks to

- **Ulf Högström, Erik Sahlee, Anna Rutgersson, Hans Bergström, Cecilia Johansson, MIUU**
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